

## FEM – deformacni pole

Celkova potencialni energie elastickeho systemu se rovna energie napjatosti materialu  $\Lambda$  mene prace externich pusobicich na teleso.

$$\Pi = \Lambda - W \quad (1)$$

pro element objemu  $dV$  je energie napjatosti dana vztahem:

$$d\Lambda = \frac{1}{2} \{\varepsilon\}^T \{\sigma\} - \frac{1}{2} \{\varepsilon_0\}^T \{\sigma\} \quad (5)$$

kde  $\{\varepsilon\}$  je vektor napjatosti,  $\{\varepsilon_0\}$  je pocatecni napjatost (nejcasteji vlivem teploty) a  $\{\sigma\}$  je vektor napeti. Celkovou energii v elementu vypocitame integraci:

$$\Lambda = \int_V \frac{1}{2} \left( \{\varepsilon\}^T \{\sigma\} - \{\varepsilon_0\}^T \{\sigma\} \right) dV \quad (6)$$

Protoze je napjatost a napeti svazano elasticckymi konstantami, muzeme proto vztah (6) zjednodusit. Napriklad pro 2D problem:

$$\{\varepsilon\}^T = [\varepsilon_r \quad \varepsilon_z \quad \varepsilon_\theta \quad \gamma_{rz}] \quad (7)$$

$$\{\sigma\}^T = [\sigma_r \quad \sigma_z \quad \sigma_\theta \quad \tau_{rz}] \quad (8)$$

a

$$\{\sigma\} = [D]\{\varepsilon\} - [D]\{\varepsilon_0\} \quad (9)$$

kde

$$[D] = \frac{E}{(1+\nu)(1-2\nu)} \begin{bmatrix} 1-\nu & \nu & \nu & 0 \\ \nu & 1-\nu & \nu & 0 \\ \nu & \nu & 1-\nu & 0 \\ 0 & 0 & 0 & \frac{1-2\nu}{2} \end{bmatrix} \quad (10)$$

energie systemu je pak:

$$\Lambda = \int_V \frac{1}{2} \left( \{\varepsilon\}^T [D]\{\varepsilon\} - 2\{\varepsilon\}^T [D]\{\varepsilon_0\} + \{\varepsilon_0\}^T [D]\{\varepsilon_0\} \right) dV \quad (11)$$

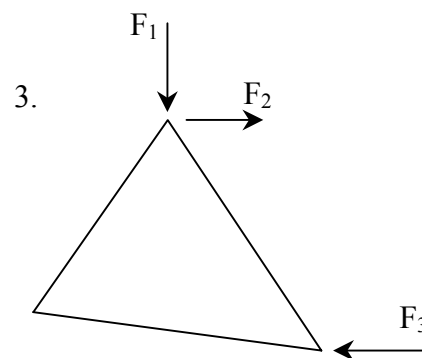
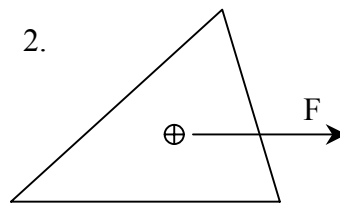
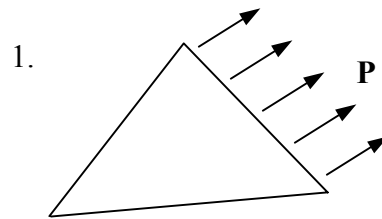
$$\{\varepsilon\} = [B]\{U\} \quad (12)$$

viz dodatek:

$$\Lambda^{(e)} = \frac{1}{2} \int_{V^{(e)}} \left( \{U^{(e)}\}^T [B^{(e)}]^T [D^{(e)}] [B^{(e)}] \{U^{(e)}\} - 2 \{U^{(e)}\}^T [B^{(e)}]^T [D^{(e)}] \{\epsilon_0^{(e)}\} + \{\epsilon_0^{(e)}\}^T [D^{(e)}] \{\epsilon_0^{(e)}\} \right) dV \quad (13)$$

Práce vykonaná externími silami může být rozdělena do tří kategorií:

1. vnitřními silami
2. práce vykonaná tlakovou zátěží
3. silami v jednotlivých uzlech



ad 1.

$$W_B^{(e)} = \int_{V^{(e)}} (uR^{(e)} + vZ^{(e)}) dV = \int_{V^{(e)}} \{U^{(e)}\}^T [N^{(e)}]^T \begin{Bmatrix} R^{(e)} \\ Z^{(e)} \end{Bmatrix} dV \quad (14)$$

kde X a Y jsou síly uvnitř elementu

ad 2.

$$W_P^{(e)} = \int_{S^{(e)}} (up_r^{(e)} + vp_z^{(e)}) dS = \int_{S^{(e)}} \{U^{(e)}\}^T [N^{(e)}]^T \begin{Bmatrix} p_r^{(e)} \\ p_z^{(e)} \end{Bmatrix} dS \quad (15)$$

$p_x$  a  $p_y$  jsou tlak(tah) na jednotlivý element

ad 3.

$$W_C^{(e)} = \{U^{(e)}\}^T \{P^{(e)}\} \quad (16)$$

$P$  vektor sil působících v uzlech elementu

Pak mohou potenciální energie elementu vypočítat podle vztahu:

$$\Pi^{(e)} = \Lambda^{(e)} - W_B^{(e)} - W_P^{(e)} - W_C^{(e)} \quad (17)$$

Potenciální energie celé soustavy je dána vztahem:

$$\Pi = \sum_{e=1}^n \Pi^{(e)} \quad (18)$$

Aby bylo těleso v rovnováze, je třeba, aby energie byla minimální

$$\frac{\partial \Pi}{\partial \{U\}} = \{0\} \quad (19)$$

tedy:

$$\begin{aligned} \{0\} = & \sum_{e=1}^n \left[ \int_{V^{(e)}} [B^{(e)}]^T [D^{(e)}] [B^{(e)}] \{U^{(e)}\} - \right. \\ & \left. - \sum_{e=1}^n \left[ \int_{V^{(e)}} [B^{(e)}]^T [D^{(e)}] \{\varepsilon_0^{(e)}\} dV + \int_{V^{(e)}} [N^{(e)}]^T \begin{Bmatrix} R^{(e)} \\ Z^{(e)} \end{Bmatrix} dV + \int_{S^{(e)}} \{U^{(e)}\}^T [N^{(e)}]^T \begin{Bmatrix} p_r^{(e)} \\ p_z^{(e)} \end{Bmatrix} dS + P^{(e)} \right] \right] \quad (20) \end{aligned}$$

nebo:

$$[K]\{U\} = \{F\} \quad (21)$$

kde:

$$[K] = \sum_{e=1}^n \left[ \int_{V^{(e)}} [B^{(e)}]^T [D^{(e)}] [B^{(e)}] \right] \quad (22)$$

a

$$\{F\} = \sum_{e=1}^n \left[ \int_{V^{(e)}} [B^{(e)}]^T [D^{(e)}] \{\varepsilon_0^{(e)}\} dV + \int_{V^{(e)}} [N^{(e)}]^T \begin{Bmatrix} R^{(e)} \\ Z^{(e)} \end{Bmatrix} dV + \int_{S^{(e)}} [N^{(e)}]^T \begin{Bmatrix} p_r^{(e)} \\ p_z^{(e)} \end{Bmatrix} dS + P^{(e)} \right] \quad (23)$$

### Vypis koeficientu matic pro nasledne programovani

Leva strava je dana soustavou integralu (22).

$$[K] = \int_V [B]^T [D][B] dV = [\underline{B}]^T [D][\underline{B}] \int_V dV = [\underline{B}]^T [D][\underline{B}] 2\pi r P \quad (24)$$

prava strana se sklada ze ctyrech casti:

Prvni cast:

$$\int_{V^{(e)}} [B^{(e)}]^T [D^{(e)}] \{\varepsilon_0^{(e)}\} dV = \frac{\alpha \Delta T E}{(1-2\nu)} [\underline{B}]^T \begin{Bmatrix} 1 \\ 1 \\ 1 \\ 0 \end{Bmatrix} 2\pi r P \quad (25)$$

$$\{\varepsilon_0\} = \alpha \Delta T \begin{Bmatrix} 1 \\ 1 \\ 1 \\ 0 \end{Bmatrix} \quad (26)$$

Druha cast:

$$\int_V [N]^T \begin{Bmatrix} R \\ Z \end{Bmatrix} dV = \int_A \begin{bmatrix} rN_i & 0 \\ 0 & rN_i \\ rN_j & 0 \\ 0 & rN_j \\ rN_k & 0 \\ 0 & rN_k \end{bmatrix} \begin{Bmatrix} R \\ Z \end{Bmatrix} 2\pi dA = \frac{\pi P}{6} \begin{Bmatrix} (2r_i + r_j + r_k)R \\ (2r_i + r_j + r_k)Z \\ (r_i + 2r_j + r_k)R \\ (r_i + 2r_j + r_k)Z \\ (r_i + r_j + 2r_k)R \\ (r_i + r_j + 2r_k)Z \end{Bmatrix} \quad (27)$$

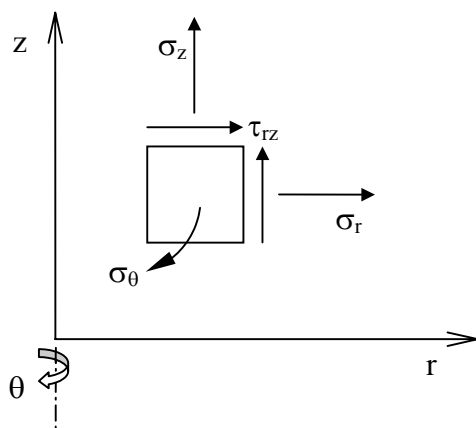
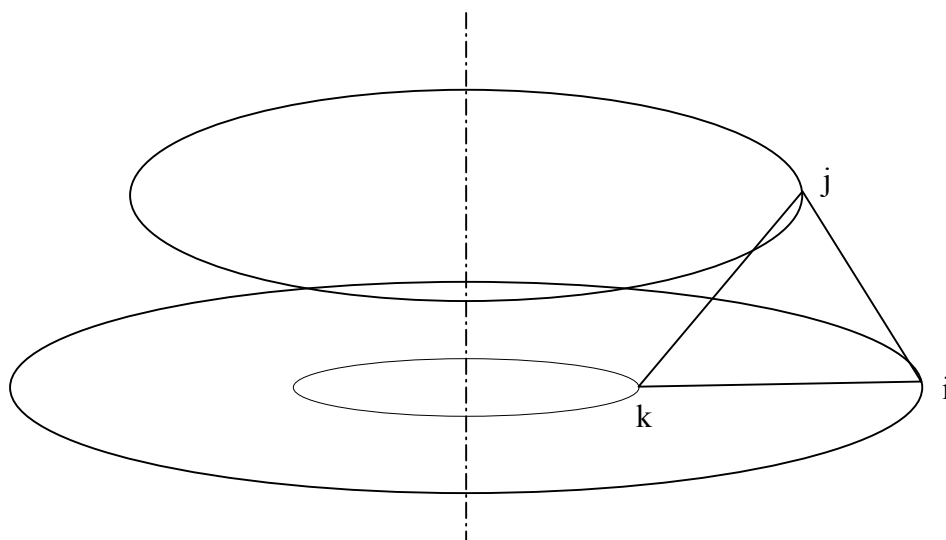
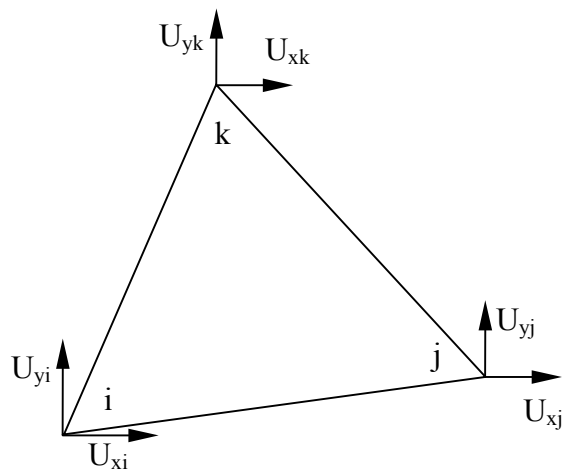
Treti cast:

$$\int_{S_{ij}} [N]^T \begin{Bmatrix} p_r \\ p_z \end{Bmatrix} dS = \int_{S_{ij}} \begin{bmatrix} N_i & 0 \\ 0 & N_i \\ N_j & 0 \\ 0 & N_j \\ N_k & 0 \\ 0 & N_k \end{bmatrix} \begin{Bmatrix} p_r \\ p_z \end{Bmatrix} dS = \int_{l_{ij}} \begin{bmatrix} N_i & 0 \\ 0 & N_i \\ N_j & 0 \\ 0 & N_j \\ 0 & 0 \\ 0 & 0 \end{bmatrix} \begin{Bmatrix} p_r \\ p_z \end{Bmatrix} 2\pi dl = \frac{l_{ij}\pi}{3} \begin{Bmatrix} (2r_i + r_j)p_r \\ (2r_i + r_j)p_z \\ (r_i + 2r_j)p_r \\ (r_i + 2r_j)p_z \\ 0 \\ 0 \end{Bmatrix} \quad (28)$$

Ctvrta cast:

vektor sil působících v uzlech trojúhelníku.

### Dodatek - triangulace



Pro zmenu polohy mohu napsat rovnice:

$$u(x,y) = \alpha_1 + \alpha_2 r + \alpha_3 z \quad (d1a)$$

$$v(x,y) = \alpha_4 + \alpha_5 r + \alpha_6 z \quad (d1b)$$

tuto rovnici mohu prepsat jako:

$$\{\delta\} = \begin{bmatrix} 1 & r & z & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & r & z \end{bmatrix} \{\alpha\} = [f] \{\alpha\} \quad (d2)$$

funkci  $\delta$  napiseme pro kazdy bod:

$$\{\delta_i\} = \begin{Bmatrix} u_i \\ v_i \end{Bmatrix} \quad (d3a)$$

$$\{\delta_j\} = \begin{Bmatrix} u_j \\ v_j \end{Bmatrix} \quad (d3b)$$

$$\{\delta_k\} = \begin{Bmatrix} u_k \\ v_k \end{Bmatrix} \quad (d3c)$$

pro cely element:

$$\{\delta^{(e)}\} = \begin{Bmatrix} \{\delta_i\} \\ \{\delta_j\} \\ \{\delta_k\} \end{Bmatrix} = \begin{Bmatrix} u_i \\ v_i \\ u_j \\ v_j \\ u_k \\ v_k \end{Bmatrix} = \begin{bmatrix} 1 & r_i & z_i & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & r_i & z_i \\ 1 & r_j & z_j & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & r_j & r_j \\ 1 & r_k & z_k & 0 & 0 & 0 \\ 0 & 0 & 0 & 1 & r_k & z_k \end{bmatrix} \begin{Bmatrix} \alpha_1 \\ \alpha_2 \\ \alpha_3 \\ \alpha_4 \\ \alpha_5 \\ \alpha_6 \end{Bmatrix} \quad (d4)$$

nebo:

$$\{\delta^{(e)}\} = [A] \{\alpha\} \quad (d5)$$

$$\{\alpha\} = [A^{-1}] \{\delta^{(e)}\} \quad (d6)$$

$$\alpha_1 = \frac{1}{2P} [(r_j z_k - r_k z_j) u_i + (r_k z_i - r_i z_k) u_j + (r_i z_j - r_j z_i) u_k] \quad (d7a)$$

$$\alpha_2 = \frac{1}{2P} [(z_j - z_k)u_i + (z_k - z_i)u_j + (z_i - z_j)u_k] \quad (d7b)$$

$$\alpha_3 = \frac{1}{2P} [(r_k - r_j)u_i + (r_i - r_k)u_j + (r_j - r_i)u_k] \quad (d7b)$$

$$\alpha_4 = \frac{1}{2P} [(r_j z_k - r_k z_j)v_i + (r_k z_i - r_i z_k)v_j + (r_i z_j - r_j z_i)v_k] \quad (d7d)$$

$$\alpha_5 = \frac{1}{2P} [(z_j - z_k)v_i + (z_k - z_i)v_j + (z_i - z_j)v_k] \quad (d7e)$$

$$\alpha_6 = \frac{1}{2P} [(r_k - r_j)v_i + (r_i - r_k)v_j + (r_j - r_i)v_k] \quad (d7f)$$

kde: P je plocha elementu

$$\begin{vmatrix} 1 & r_i & z_i \\ 1 & r_j & z_j \\ 1 & r_k & z_k \end{vmatrix} = 2P \quad (d8)$$

dosazenim (d7a), (d7b), (d7c), (d7d), (d7e) a (d7f) do rovnice (d2) ziskame rovnici:

$$\begin{Bmatrix} u \\ v \end{Bmatrix} = \{\delta\} = \begin{bmatrix} N_i & 0 & N_j & 0 & N_k & 0 \\ 0 & N_i & 0 & N_j & 0 & N_k \end{bmatrix} \begin{Bmatrix} u_i \\ v_i \\ u_j \\ v_j \\ u_k \\ v_k \end{Bmatrix} = [N]\{U\} \quad (d9)$$

$$\text{kde: } N_i = \frac{1}{2P} [a_i + b_i x + c_i y] \quad a_i = r_j z_k - r_k z_j \quad (d10a)$$

$$b_i = z_j - z_k$$

$$c_i = r_k - r_j$$

$$N_j = \frac{1}{2P} [a_j + b_j x + c_j y] \quad a_j = r_k z_i - r_i z_k \quad (d10b)$$

$$b_j = z_k - z_i$$

$$c_j = r_i - r_k$$

$$N_k = \frac{1}{2P} [a_k + b_k x + c_k y] \quad a_k = r_i z_j - r_j z_i \quad (d10c)$$

$$b_k = z_i - z_j$$

$$c_k = r_j - r_i$$



casto je znat derivaci:

$$\{\varepsilon\} = \begin{Bmatrix} \varepsilon_r \\ \varepsilon_z \\ \varepsilon_\theta \\ \gamma_{xy} \end{Bmatrix} = \begin{Bmatrix} \frac{\partial u}{\partial r} \\ \frac{\partial v}{\partial z} \\ \frac{u}{r} \\ \frac{\partial u}{\partial y} + \frac{\partial v}{\partial x} \end{Bmatrix} = \quad (d11)$$

$$= \frac{1}{2P} \begin{bmatrix} b_i & 0 & b_j & 0 & b_k & 0 \\ 0 & c_i & 0 & c_j & 0 & c_k \\ \frac{a_i}{r} + b_i + c_i \frac{z}{r} & 0 & \frac{a_j}{r} + b_j + c_j \frac{z}{r} & 0 & \frac{a_k}{r} + b_k + c_k \frac{z}{r} & 0 \\ c_i & b_i & c_j & b_j & c_k & b_k \end{bmatrix} \begin{Bmatrix} u_i \\ v_i \\ u_j \\ v_j \\ u_k \\ v_k \end{Bmatrix} = [B]\{U\}$$

Pouzita literatura:

- [1] Larry J. Segerlind, Applied Finite Element Analys, Wiley&Sons, New York,1976
- [2] O. C. Zienkiewicz, The Finite Element Method (third edition), McGRAW-HILL Book Company, UK, 1977
- [3] M. J. Fagan, Finite Element Analysis, Longman Group UK, 1992